# Chance Constraints for Improving Security of AC Optimal Power Flow

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# Renewable energy increases *variability* and *uncertainty* in power systems operation.



#### How to limit adverse impacts of uncertainty?



#### **Chance-Constrained** Optimal Power Flow

Limit probability of constraint violations



#### Chance-Constrained AC Optimal Power Flow

Non-linear dependence on uncertain variables!

- 1. AC Power Flow and System Response to Uncertainty
- 2. Chance-Constrained AC Optimal Power Flow
- 3. Handling Quadratic Chance Constraints
- 4. Numerical Results
- 5. Summary and Conclusion

Two **equations** per bus: Nodal power balance equations for *active* and *reactive* power



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#### Four variables per bus:

- p active power
- q reactive power
- v voltage magnitude
- $\theta$  Voltage angle

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**Choose** two variables per bus: *pq* bus - load buses *pv* bus - local voltage control *θv* bus - reference bus/slack bus

# **AC OPTIMAL Power Flow**

min 
$$\sum_{i \in \mathcal{G}} c_{G,i}(p_{G,i})$$
  
s.t.  $F(f^p, f^q, \theta, v, p, q) = 0$   
 $p_G^{min} \le p_G \le p_G^{max}$   
 $q_G^{min} \le q_G \le q_G^{max}$   
 $v^{min} \le v \le v^{max}$   
 $\sqrt{(f^p)^2 + (f^q)^2} \le s^{max}$   
 $\theta_{\theta V} = 0$ 

Minimize generation cost

Nodal power balance Active generation Reactive generation Voltage magnitudes Power flows

Not really necessary to differ between pq, pv and  $\theta v$  buses. But - influences system response under uncertainty!

# **Modeling Uncertainty**

• Active power  $= p + \omega$ 

p - forecasted active power  $\omega$  - random fluctuation

- Reactive power =  $q + \gamma \omega$ 
  - q forecasted reactive power  $\gamma\omega$  constant power factor



Consumed and produced power must be balanced at all times!

- **Balanced** for  $\omega = 0$
- Active power Automatic Generation Control (AGC) [Borkowska 1974], [Vrakopoulou 2013]

 $p_{G}^{new} = p_{G} - \alpha \left(\sum \omega\right)$ 

• Reactive power - Local voltage control at PV buses

 $v_i = const$ , adjust reactive power  $q_G^{new}$  to achieve this!

#### Generator active power

$$\mathbb{P}(p_{G,i} \underbrace{-\alpha_{i}\left(\sum_{\substack{\omega \\ \sigma_{G,i}}} \omega\right)}_{\mathsf{RESERVE}} \leq p_{G,i}^{\mathsf{max}}) \geq 1 - \epsilon$$

Insufficient reserves

# $\begin{array}{l} \textbf{Generator reactive power} \\ \mathbb{P}\left(q_{\textit{G},i}(\omega) \leq q_{\textit{G},i}^{\max}\right) \geq 1 - \epsilon \end{array}$

Voltages change

#### Voltage magnitudes

$$\mathbb{P}\left(v_i(\omega) \leq v_i^{\max}\right) \geq 1 - \epsilon$$

Voltages out of bound

#### **Power flows**

$$\mathbb{P}\left(\sqrt{(f_{ij}^p(\omega))^2 + (f_{ij}^q(\omega))^2} \le s^{max}\right) \ge 1 - \epsilon \quad \text{Temp. overload/redispatch}$$

Non-linear uncertainty quantification + optimization friendliness

Some approaches:

- Linear DC power flow approximation [Vrakopoulou et al 2012], [Roald et al 2013], [Bienstock, Chertkov and Harnett 2014], [Lubin, Dvorkin, Backhaus 2016]
- SDP relaxation, sample-based reformulation [Vrakopoulou et al 2013]
- Full AC equations for ω = 0, linearized uncertainty [Qu, Roald, Andersson 2015], [Schmidli et al 2016]
- Linearized AC power flow with voltage constraints [Baker, Summers, Dall'Anese 2016]

Goal: Include power flow constraints and optimized response!

Power injections are **not** Gaussian.

Power flows are typically close to Gaussian.

$$\mathbb{P}\left(\sqrt{(f_{ij}^p(\omega))^2 + (f_{ij}^q(\omega))^2} \le s^{max}\right) \ge 1 - \epsilon$$

Depends on high-dimensional random vector  $\rightarrow$  "Central limit theorem"!

We don't know how to impose chance constraints directly on ACOPF. Known tractable methods require a linear relationship between injections, voltages, and flows.

So we propose to...

- 1. Solve deterministic AC OPF
- 2. Linearize around solution point.
- 3. Solve convex optimization problem with chance constraints.

Let  $x := (f^p, f^q, \theta, v, p, q)$ , so that the AC equations can be expressed as

$$F(x)=0.$$

Given a feasible operating point  $\tilde{x} := (\tilde{f}^p, \tilde{f}^q, \tilde{\theta}, \tilde{v}, \tilde{p}, \tilde{q})$ , we instead enforce the linear equations

$$\nabla F(\tilde{x})^T(x-\tilde{x})+F(\tilde{x})=0.$$

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Can be inverted to obtain flows  $(f^p, f^q)$  as affine function of voltages and injections  $(\theta, v, p, q)$ .

Recall line flow constraints

$$\sqrt{(f^p)^2+(f^q)^2}\leq s^{max}$$

Using (approximate) linear relationship, to impose line flow constraints we end up with chance constraints of the form

$$\mathbb{P}_{\xi}\left((a^{T}\xi+b)^{2}+(c^{T}\xi+d)^{2}\leq k
ight)\geq1-\epsilon$$

where *a*, *b*, *c*, *d* are decision variables

Is this a convex constraint?

Not convex for  $\epsilon = 0.445$ 

$$P((x\xi_1)^2 + (y\xi_2)^2 \le 1) \ge 1 - \epsilon$$



х

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$$P((x\xi_1)^2 + (y\xi_2)^2 \le 1) \ge 1 - \epsilon$$

Counterexample does not apply for smaller  $\epsilon,$  but anyway let's look for approximations

Start off by trying to understand the simpler (previously unstudied) constraint

$$\mathbb{P}(\mathbf{a} \le \mathbf{x}^{\mathsf{T}} \boldsymbol{\xi} \le \mathbf{b}) \ge 1 - \epsilon$$

where  $a \in \mathbb{R}$ ,  $b \in \mathbb{R}$ , and  $x \in \mathbb{R}^n$  are decision variables, and  $\xi$  is jointly Gaussian with known mean and covariance

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**Result:** The "two-sided" chance constraint above defines a convex set in (a, b, x) when  $\epsilon \leq \frac{1}{2}$  (L., Bienstock. Vielma, 2016)

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But representation requires perspective transformation, so nonsmooth. Not representable using standard cones.

# $\mathbf{2}\epsilon$ outer approximation



- With two linear constraints plus second-order cone, we guarantee that chance constraint holds with 2e. (Can be made conservative)
- Proof: split into two linear chance constraints P(a ≤ x<sup>T</sup>ξ) ≥ 1 − ε, P(x<sup>T</sup>ξ ≤ b) ≥ 1 − ε

# $1.25\epsilon$ outer approximation



- With three linear constraints plus second-order cone, we guarantee that chance constraint holds with  $1.25\epsilon$
- Proof: L., Bienstock, Vielma (2016)

Fix  $\epsilon < \frac{1}{2}$  and  $\beta \in (0, 1)$ . If  $\exists f_1, f_2$  such that

$$\begin{split} \mathbb{P}(|a^T\xi + b| \le f_1) \ge 1 - \beta \epsilon \\ \mathbb{P}(|c^T\xi + d| \le f_2) \ge 1 - (1 - \beta) \epsilon \\ f_1^2 + f_2^2 \le k \end{split}$$

then

$$\mathbb{P}\left((\boldsymbol{a}^{\mathsf{T}}\boldsymbol{\xi}+\boldsymbol{b})^2+(\boldsymbol{c}^{\mathsf{T}}\boldsymbol{\xi}+\boldsymbol{d})^2\leq k\right)\geq 1-\epsilon$$

Proof: Union bound

So this gives us a convex, tractable (via SOCP) approximation for

$$\mathbb{P}\left((a^T\xi+b)^2+(c^T\xi+d)^2\leq k
ight)\geq 1-\epsilon$$

What about other approaches?

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What about other approaches?

- Robust optimization ( $\rightarrow$  SDP)
- CVaR (sampling)

- 1. Solve deterministic ACOPF (using local nonlinear solver)
- 2. Linearize around that solution, add chance constraints
- 3. Solve convex problem (SOCP) to obtain new production levels p, qand response parameters  $\alpha$ , etc
- Given realization of uncertainty (in sample), solve feasibility problem with injections fixed to check if computed solution induces feasible flows and voltages

**Table 1:** Comparison of Feasibility (%) Against In-Sample UncertaintyRealizations (1000 samples)

ε	$10^{-1}$	10 <sup>-2</sup>	10 <sup>-3</sup>
ACOPF ( $\alpha_i = 1/N_g$ )	0.073	0.076	0.076
ACOPF (cheating)	53.0	53.4	53.4
CCACOPF ( $\alpha_i = 1/N_g$ )	84.1	97.4	99.8
CCACOPF (opt)	85.4	98.6	99.8

Test system: IEEE RTS96 three area

#### There's modeling software too!

github.com/kersulis/IJulia-WPS

github.com/mlubin/JuMPChance.jl

jumpchance.readthedocs.io/en/latest/twoside.html

- Preliminary results show that deterministic ACOPF + linearization + chance constraints can give more "robust" solutions than determistic ACOPF.
- Very little additional computational overhead compared with solving determistic ACOPF alone
- Can be used to study reactive power generation response policies.
- Lots of room to experiment and expand on the methodology.

#### Thanks!