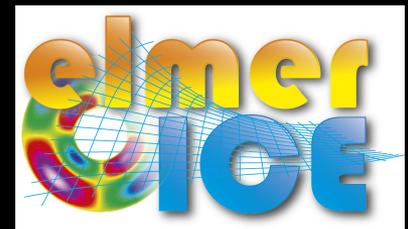


Friction at the base of glaciers: insights from modeling at various scales

Olivier Gagliardini, Julien Brondex, Fabien Gillet-Chaulet

Mathematical Modelling in Glaciology BIRS workshop
Banff, January 2020



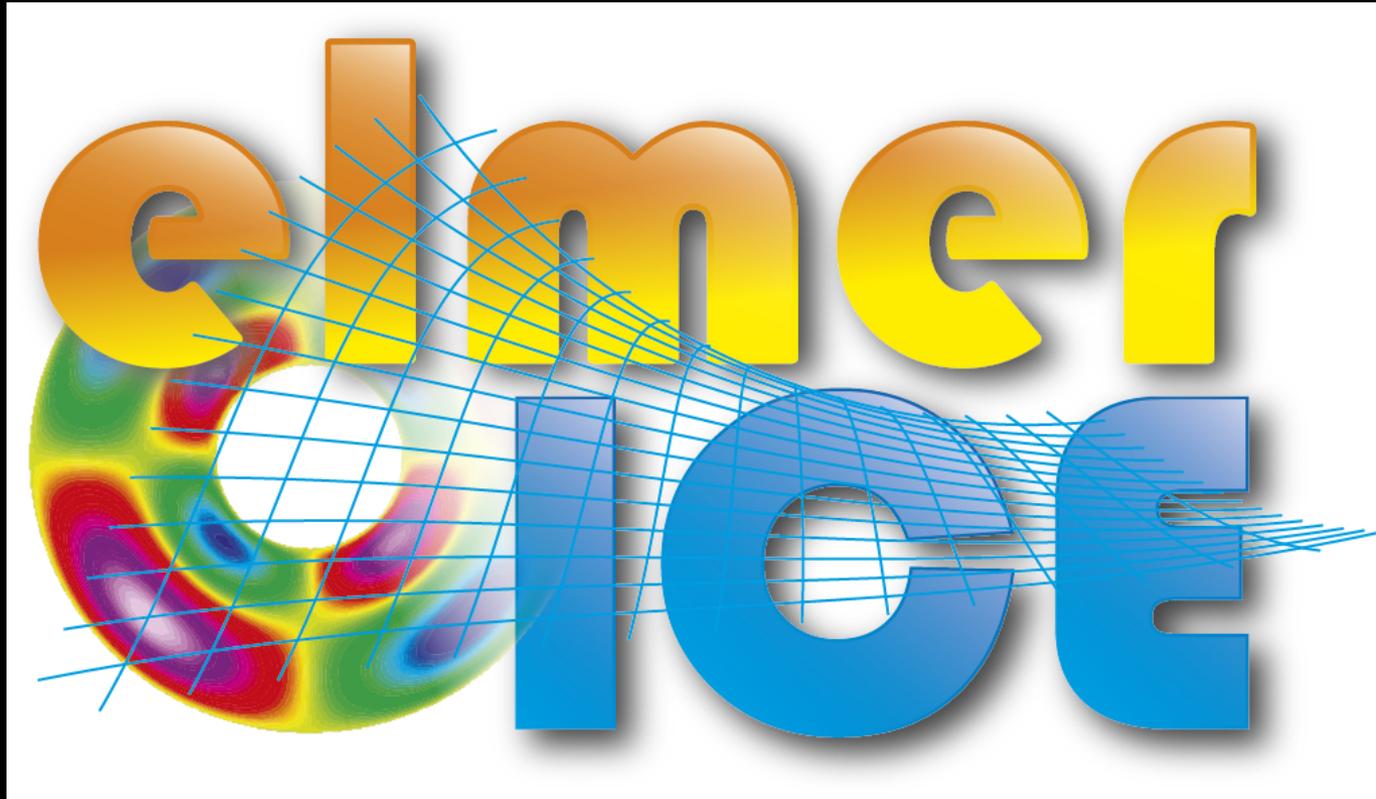
Two scales - two parts

1/ micro-meso scale: friction law formulation

2/ macro scale: grounding line sensitivity to the choice of the friction law

A unique modelling tool: Elmer/Ice

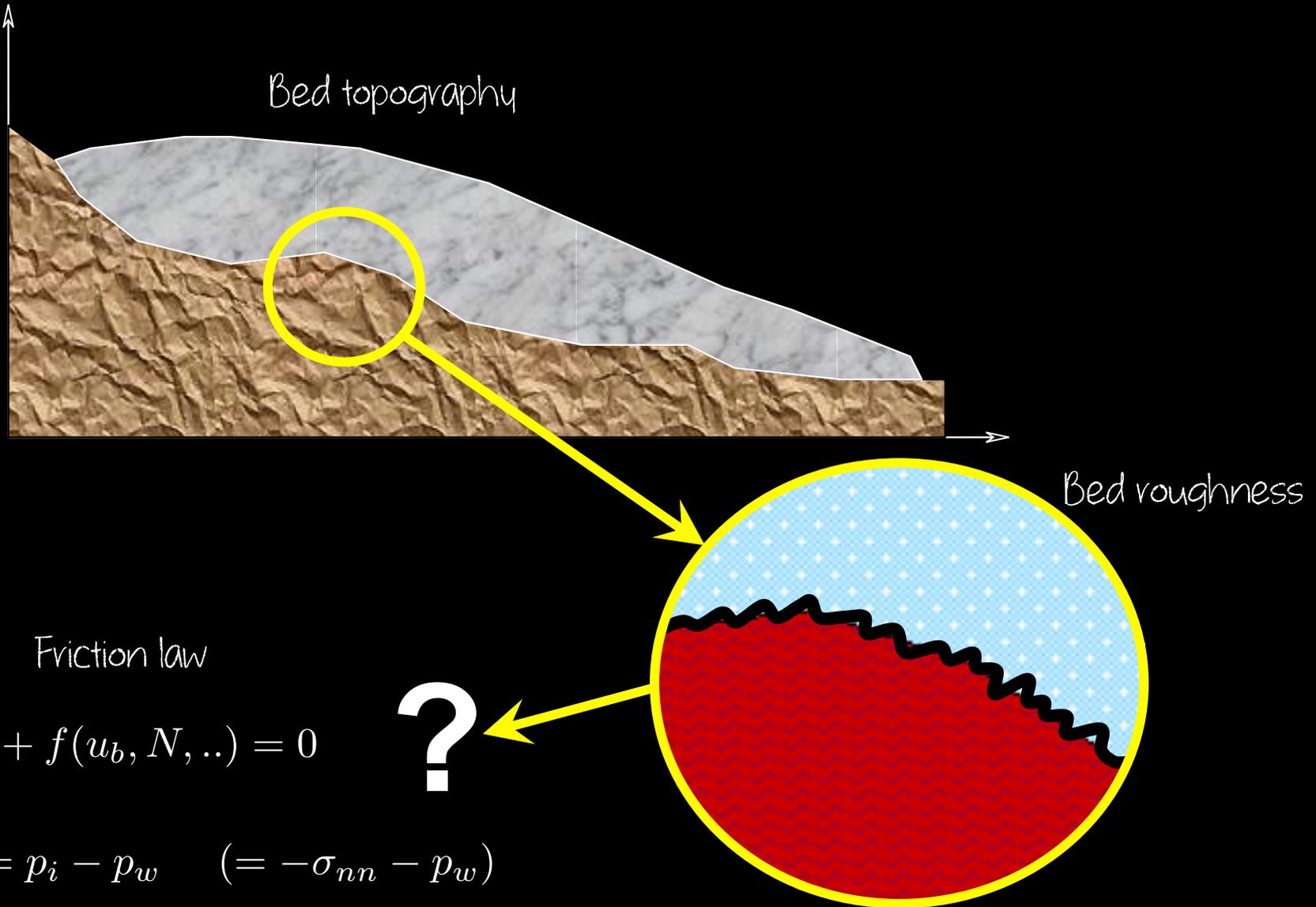
Open Source Finite Element Software for Ice Sheet, Glaciers and Ice Flow Modelling



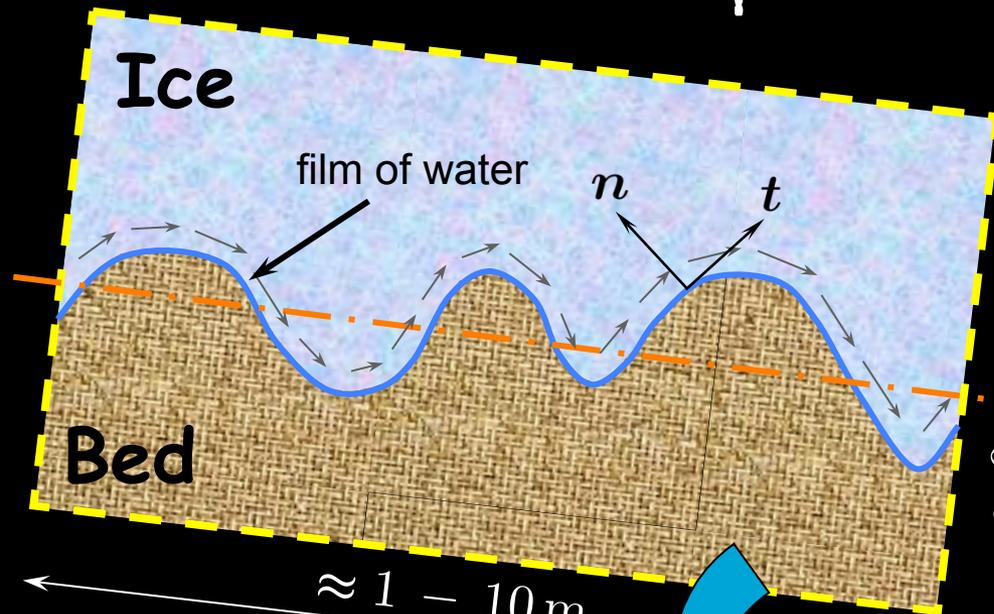
<http://elmerice.elmerfem.org/>

Concept of friction law
in Glaciology
and role of water

Bed topography / roughness

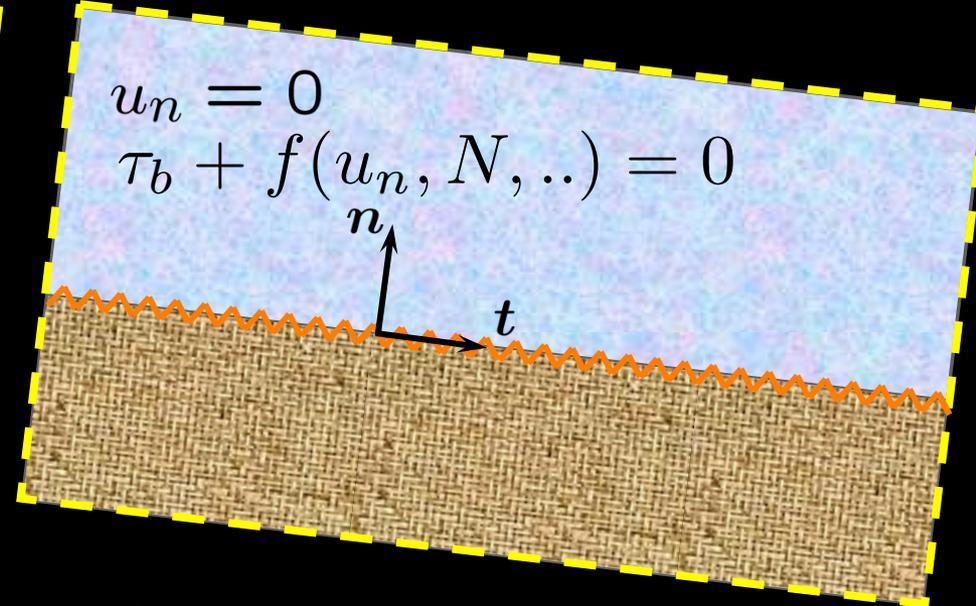


Concept of friction law



$\approx 0.1 - 1 \text{ m}$

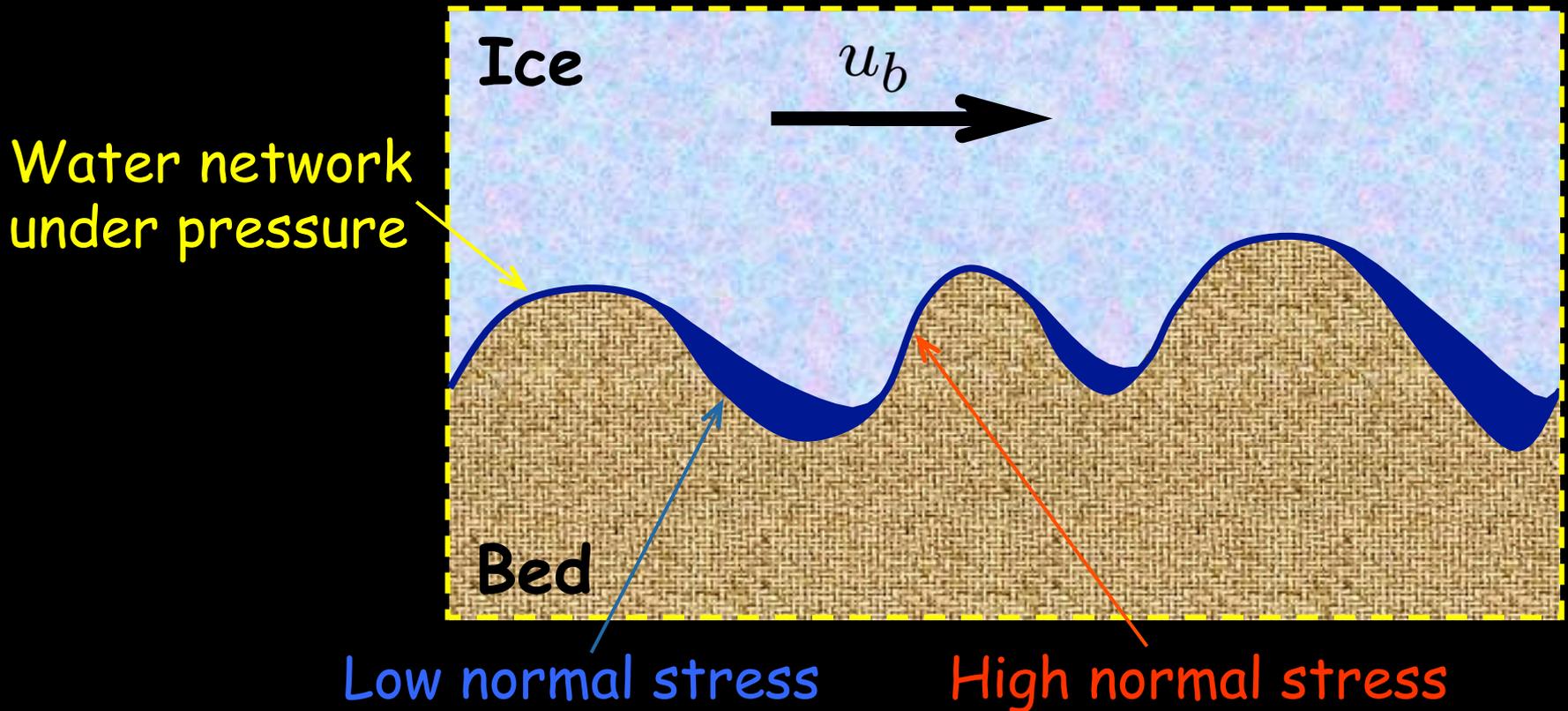
$u_n = 0$ hard bed
 $\sigma_{nt} = 0$ free slip



[Weertman (1957), Fowler (1981), Gudmundsson (1997)]

Effect of water

If water pressure and/or velocity increase



➔ What is the form of the friction law ?

$$\tau_b - f(u_b, N, \dots) = 0$$

A bit of history...

Journal of Glaciology, Vol. 56, No. 200, 2010

Weertman, Liboutry and the development of sliding theory

A.C. FOWLER

read more: <https://saussure.osug.fr/-History->

Johannes 'Hans' Weertman (1925-2018)



1957, JoG

ON THE SLIDING OF GLACIERS

By J. WEERTMAN

(Naval Research Laboratory, Washington, D.C.)

ABSTRACT. A model is proposed to explain the sliding of any glacier whose bottom surface is at the pressure melting point. Two mechanisms are considered. One is pressure melting and the other is creep rate enhancement through stress concentrations. Neither of the mechanisms operating alone is sufficient to explain sliding. If both mechanisms operate together appreciable sliding can occur.

RÉSUMÉ. On propose un modèle pour expliquer le glissement d'un glacier dont le fond se maintient au point de fusion. On considère deux mécanismes : le fusion de pression et l'augmentation de la vitesse de déformation causée par les concentrations de tension. Ni l'un ni l'autre en agissant seul ne suffit à expliquer le glissement. Mais ensemble ils occasionneraient un glissement assez important.

2 mechanisms:

- pressure melting/refreezing
- creep rate enhancement

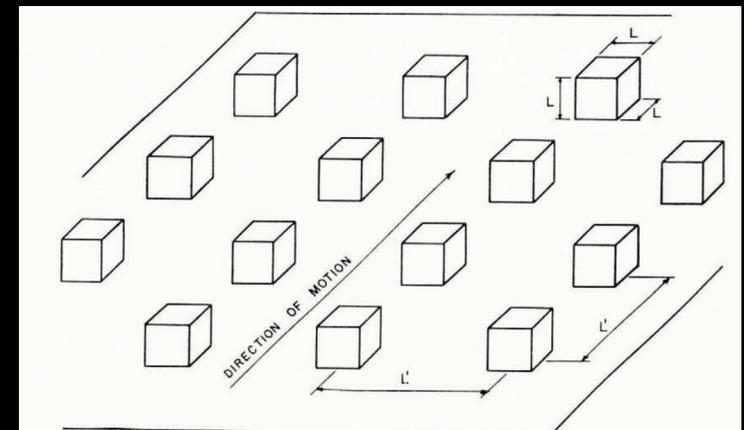


Fig. 1. Idealized glacier bed

Louis Lliboutry (1922-2007)



1958, CRAS (in French)

GLACIOLOGIE. — *Contribution à la théorie du frottement du glacier sur son lit.*

Note (*) M. **LOUIS LLIBOUTRY**, présentée par M. Léon Moret.

L'introduction d'un troisième mécanisme de franchissement des protubérances permet d'expliquer l'indépendance du frottement dynamique vis-à-vis de la vitesse, la valeur plus élevée du frottement statique (et donc le mouvement par saccades), l'accélération du glacier aux époques chaudes, et enfin l'usure caractéristique qui conduit à des roches moutonnées.

3rd mechanisms:

opening of **cavities** on the lee side of bed bumps

Liboutry will publish more than 20 papers on that specific subject!

This one in 1968 :

Journal of Glaciology, Vol. 7, No. 49, 1968

GENERAL THEORY OF SUBGLACIAL CAVITATION AND
SLIDING OF TEMPERATE GLACIERS

By L. LLIBOUTRY

(Laboratoire de Glaciologie du C.N.R.S., Grenoble, Isère, France)

followed by one from Weertman in 1972:

REVIEWS OF GEOPHYSICS AND SPACE PHYSICS, VOL. 10, NO. 1, PP. 287-333, FEBRUARY 1972

**General Theory of Water Flow at the Base of a
Glacier or Ice Sheet**

J. WEERTMAN

*Scott Polar Research Institute
Cambridge, England CB2 1ER*

read more: <https://saussure.osug.fr/-History->

10 march 2005, SHF, Grenoble

S.H.F. Section de Glaciologie-Nivologie. Réunion du 10 Mars 2005

Glissement et hydraulique sous-glaciaires

Louis LLIBOUTRY

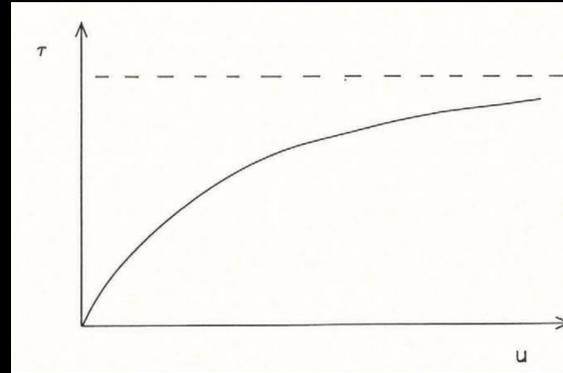
3, Av. de la Foy, Corenc, 38700 La Tronche

Llibourty : "..., on en est resté aux théories grossières, incomplètes et erronées émises dans les années 60 par Weertman, moi-même, Nye, Röthlisberger, et Budd, qui n'ont plus qu'un intérêt historique aujourd'hui."

He presented a new theory (in 10 minutes) which should be published in 3 papers that he was about to submit to Journal of Glaciology

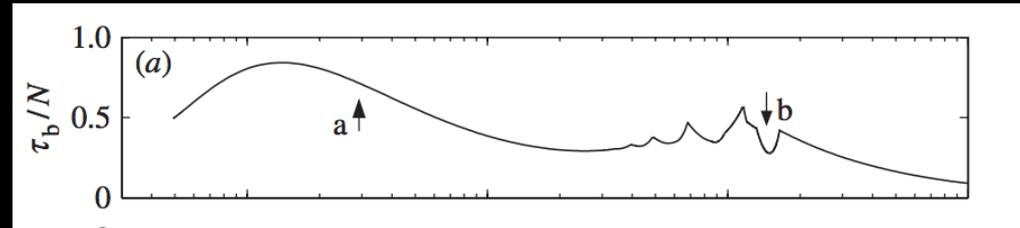
These papers will never be submitted... and the manuscripts are lost...

Fowler, 1981, 1987



Schoof 2005

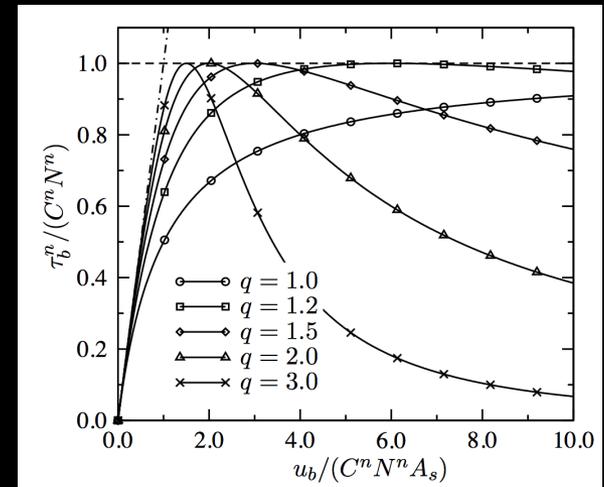
$$\frac{\tau_b}{N} = C \left(\frac{\Lambda}{\Lambda + \Lambda_0} \right)^{1/n}, \quad \Lambda = \frac{u_b}{N^n}$$



Gagliardini et al., 2007

$$\frac{\tau_b}{CN} = \left(\frac{\chi}{1 + \alpha \chi^q} \right)^{1/n}$$

$$\chi = \frac{u_b}{A_s C^n N^n}; \quad \alpha = \frac{(q-1)(q-1)}{q^q}$$



All these formulations are based on strong assumptions:

- **two-dimensional bed geometry** see Helanow et al., GRL 2019

- **pure sliding at the interface**

wait for Roldan Blasco et al. , in preparation

- **steady water pressure** **This talk!**

and

- **have not yet been validated against real data**

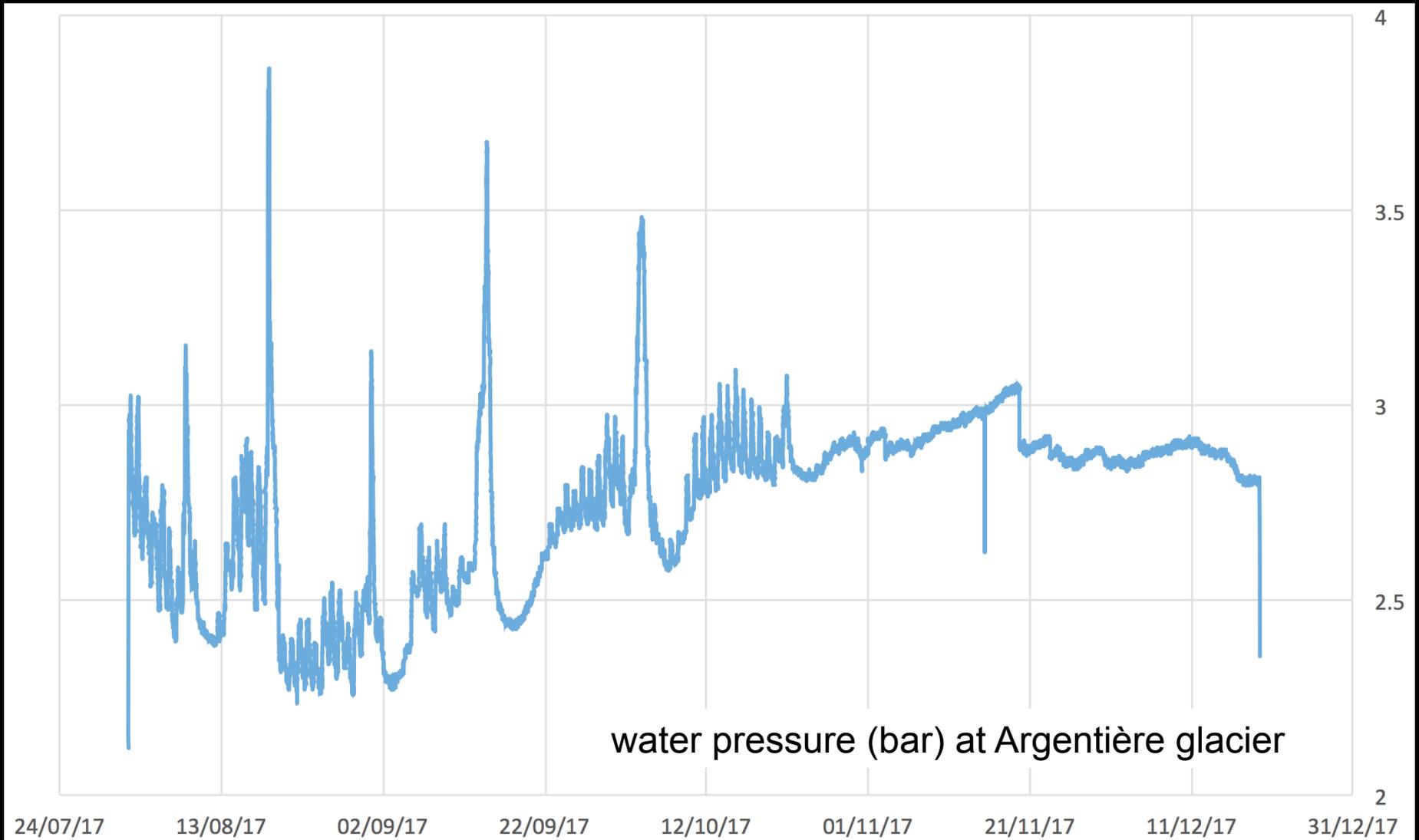
wait for Gimbert et al. , submitted

- **their link with basal hydrology is still unclear**

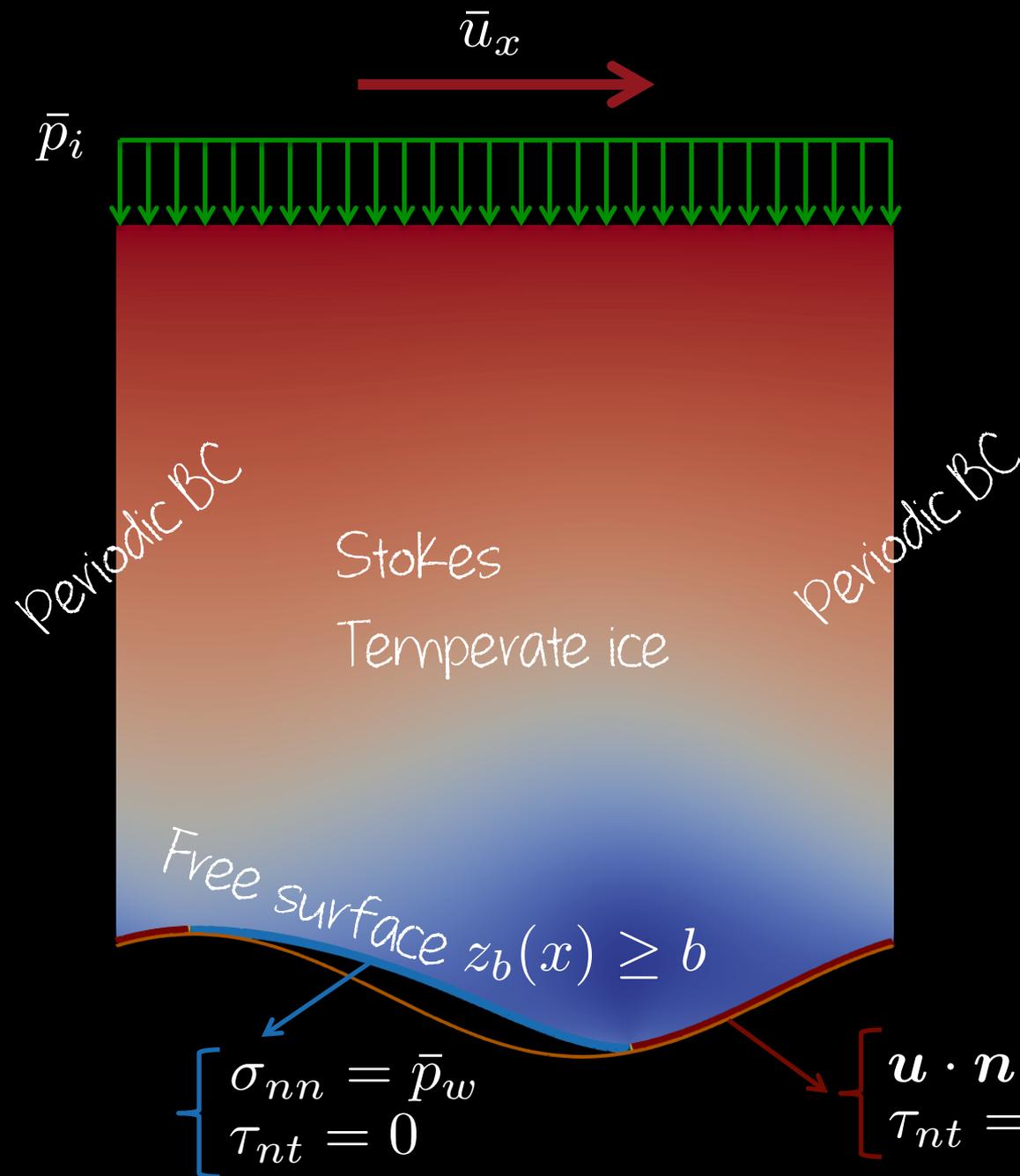
wait for Gilbert et al. in preparation

How these laws are modified if
water pressure at the base is
unsteady?

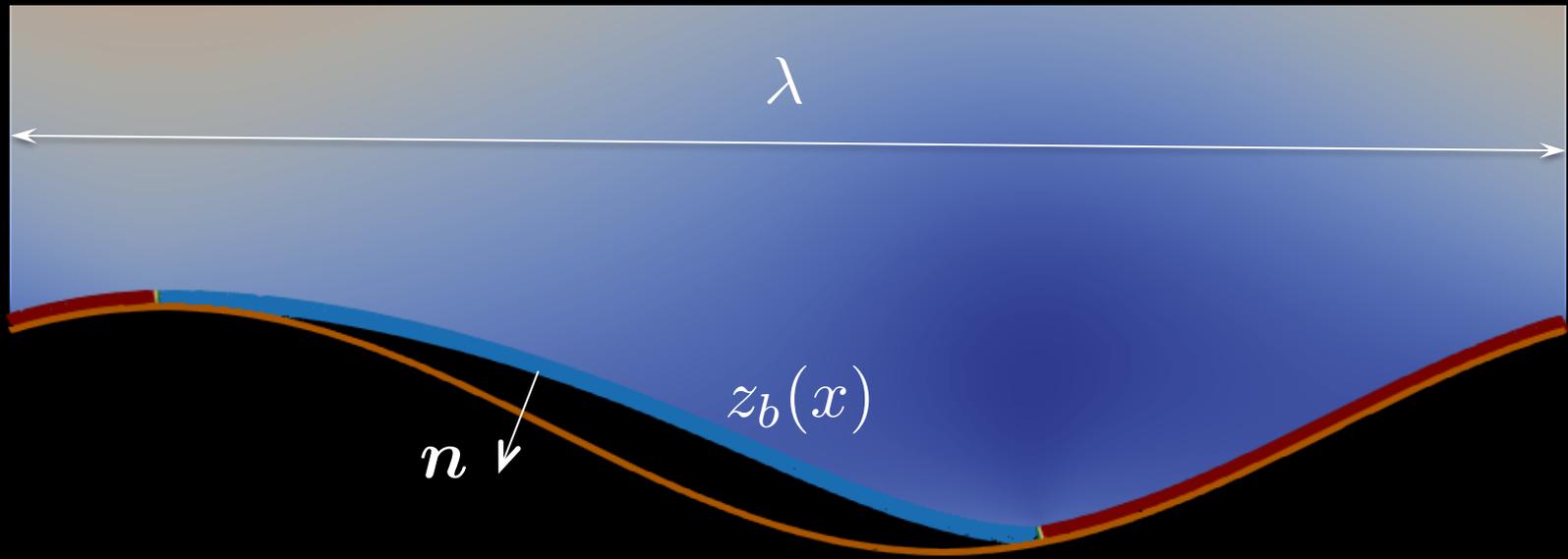
and water pressure is not steady...



water pressure (bar) at Argentière glacier



For given \bar{p}_i and \bar{u}_x
evolve \bar{p}_w / \bar{p}_i
and look for
steady state



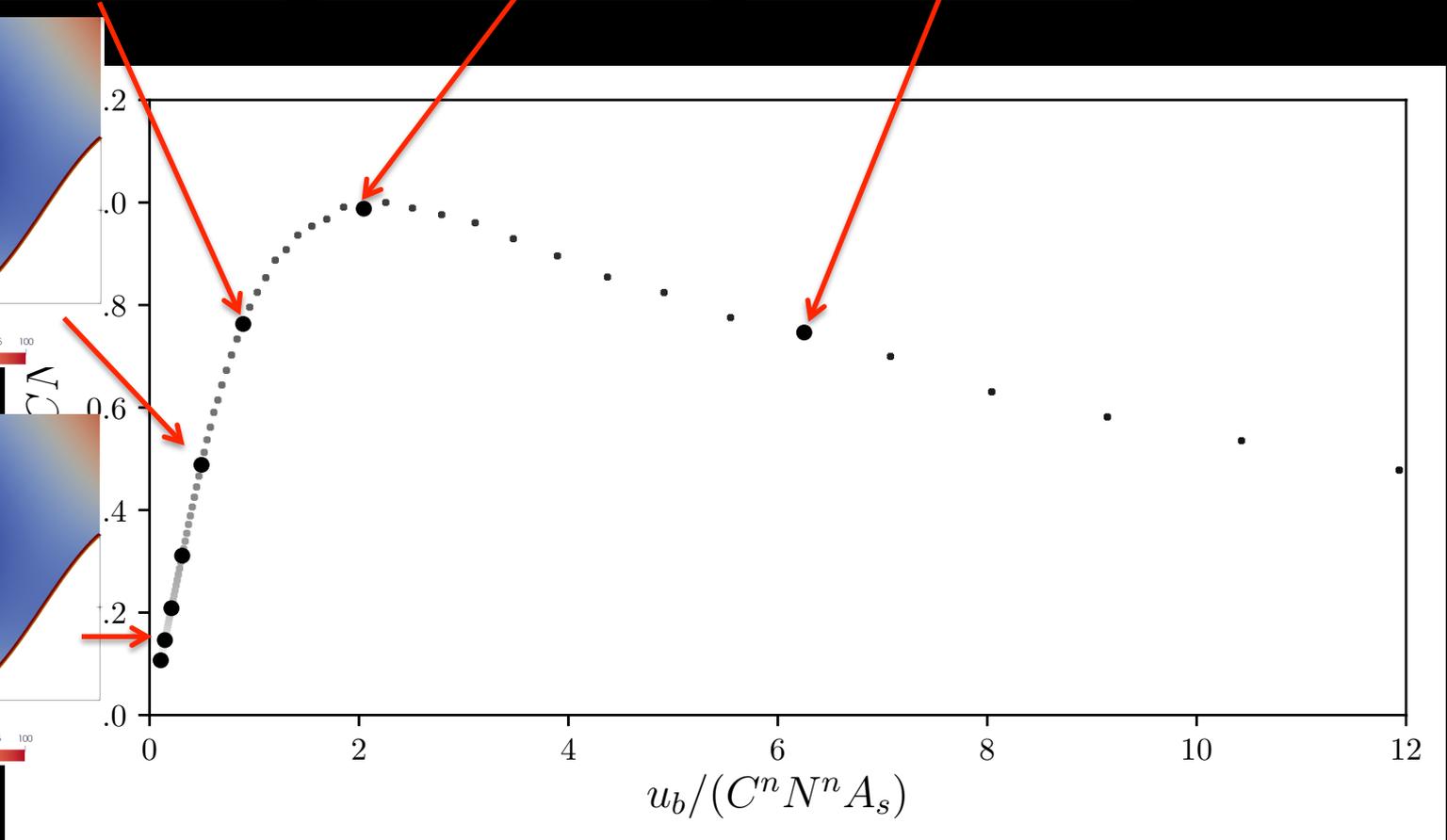
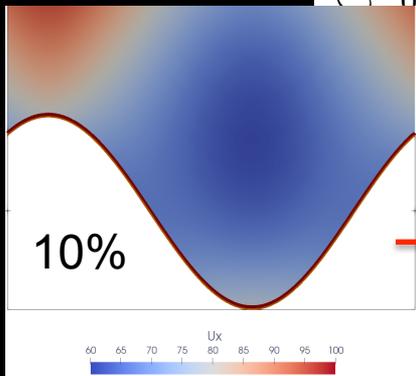
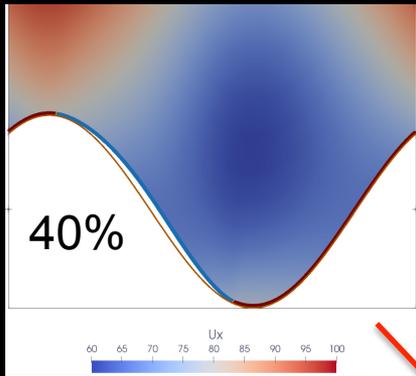
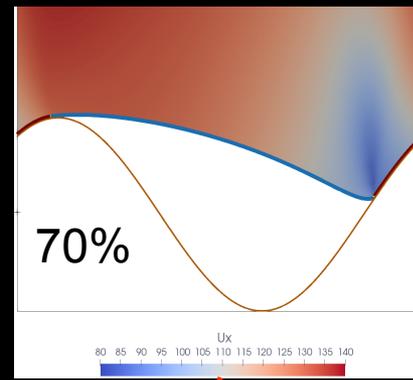
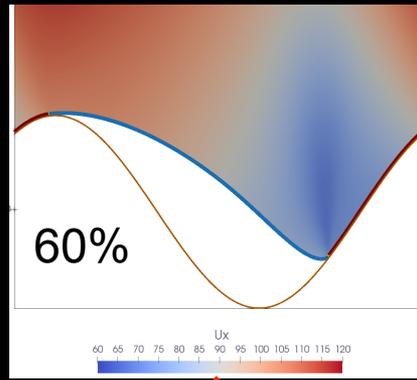
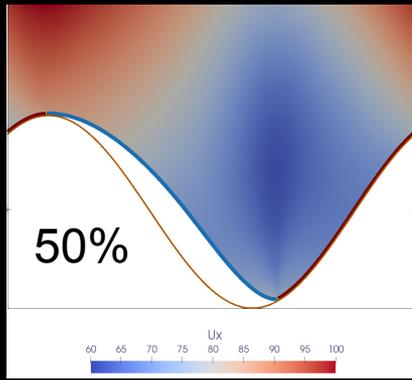
$$\left. \begin{aligned} \tau_b &= \frac{1}{\lambda} \int_0^\lambda \sigma_{nn} n_x ds = \frac{1}{\lambda} \int_0^\lambda \sigma_{nn} \frac{\partial z_b}{\partial x} dx \\ u_b &= \frac{1}{\lambda} \int_0^\lambda u dx \end{aligned} \right\} \rightarrow \tau_b = f(u_b, N)$$

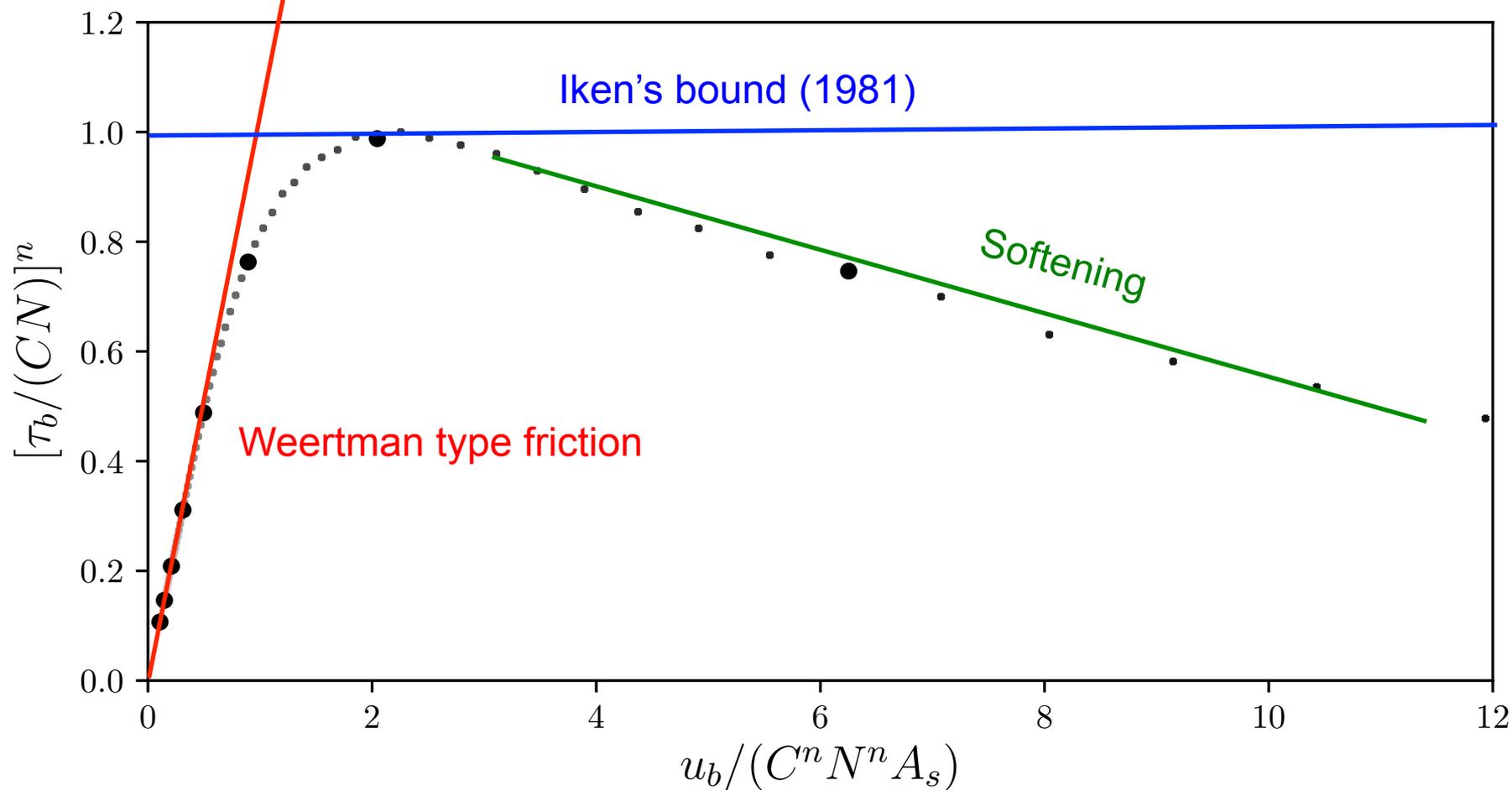
$$N = p_i - \bar{p}_w$$

$$p_i = \frac{1}{\lambda} \int_0^\lambda \sigma_{nn} n_y ds = -\frac{1}{\lambda} \int_0^\lambda \sigma_{nn} dx \approx \bar{p}_i$$



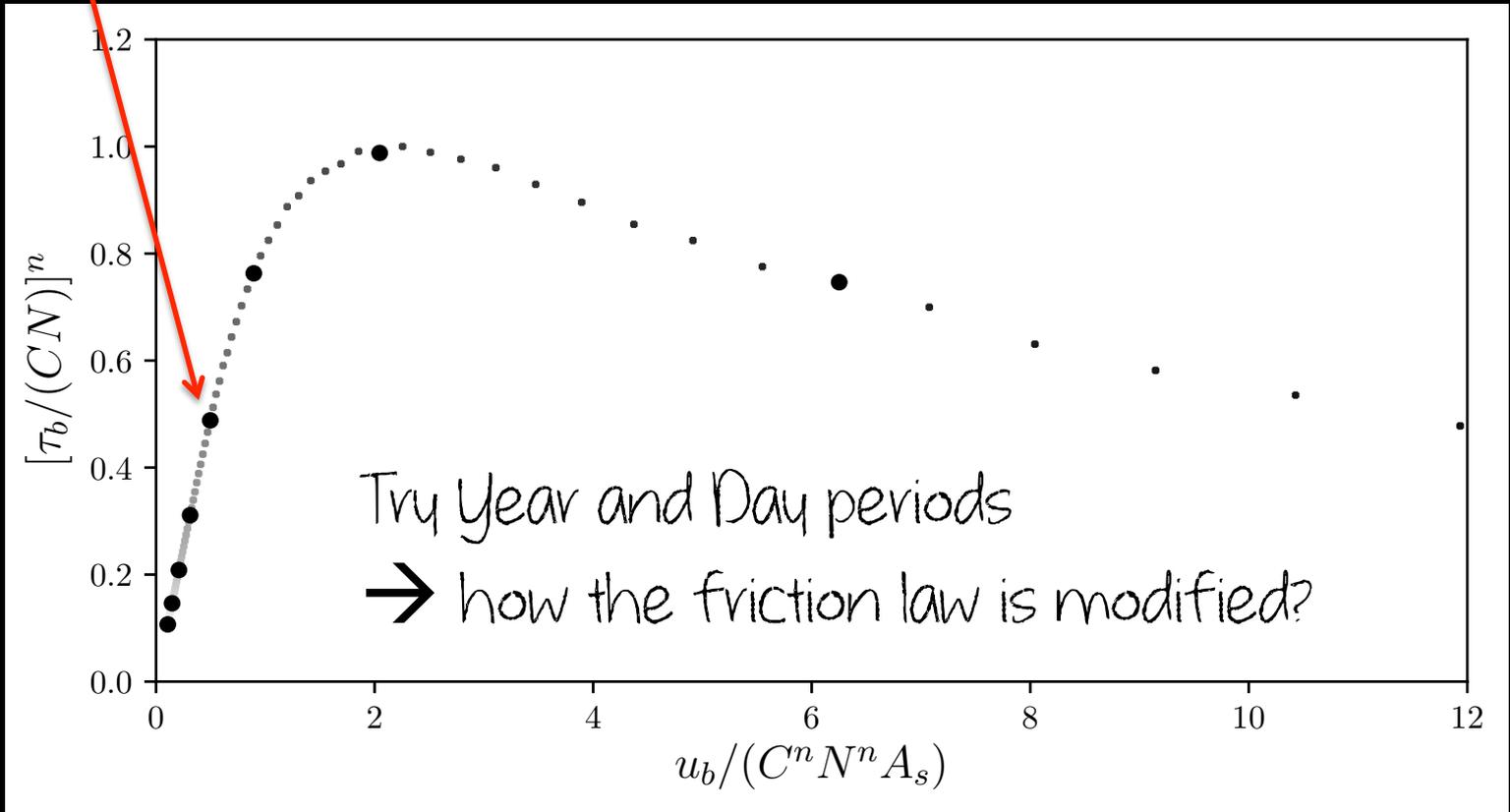
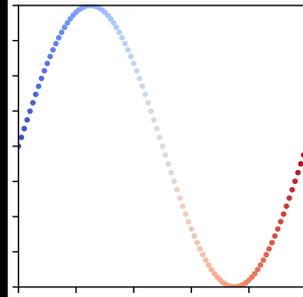
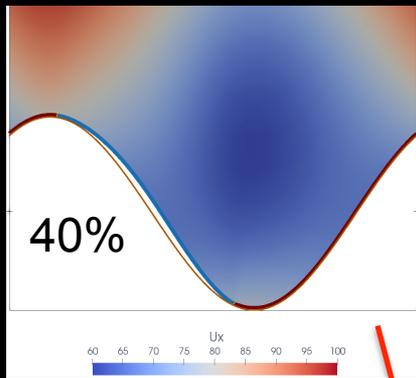
\bar{p}_w / \bar{p}_i





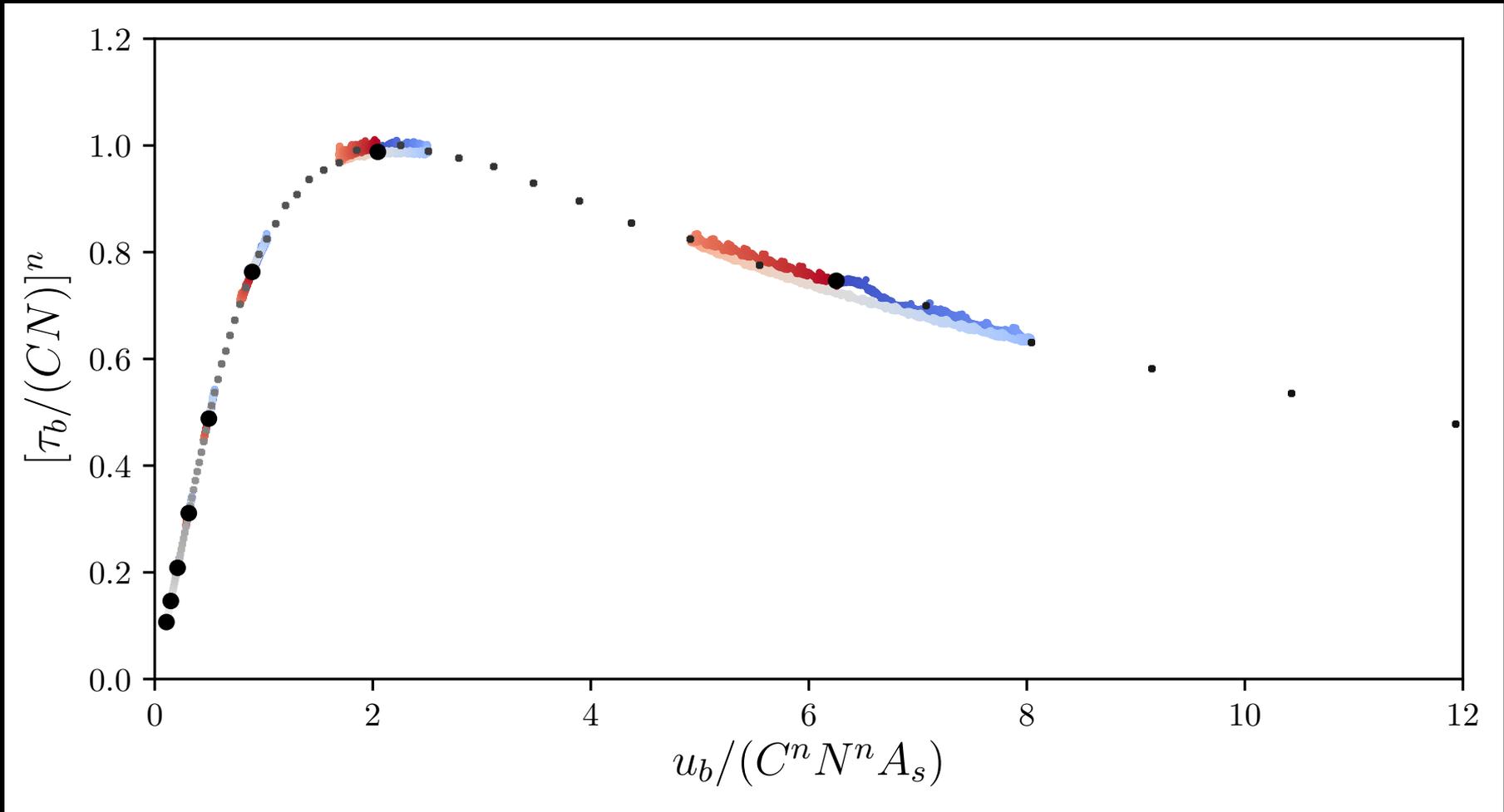
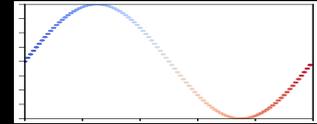
$$p_w(t) = \bar{p}_w + \Delta p_w \sin(\omega t)$$

$$\Delta p_w / \bar{p}_i = 2\%$$



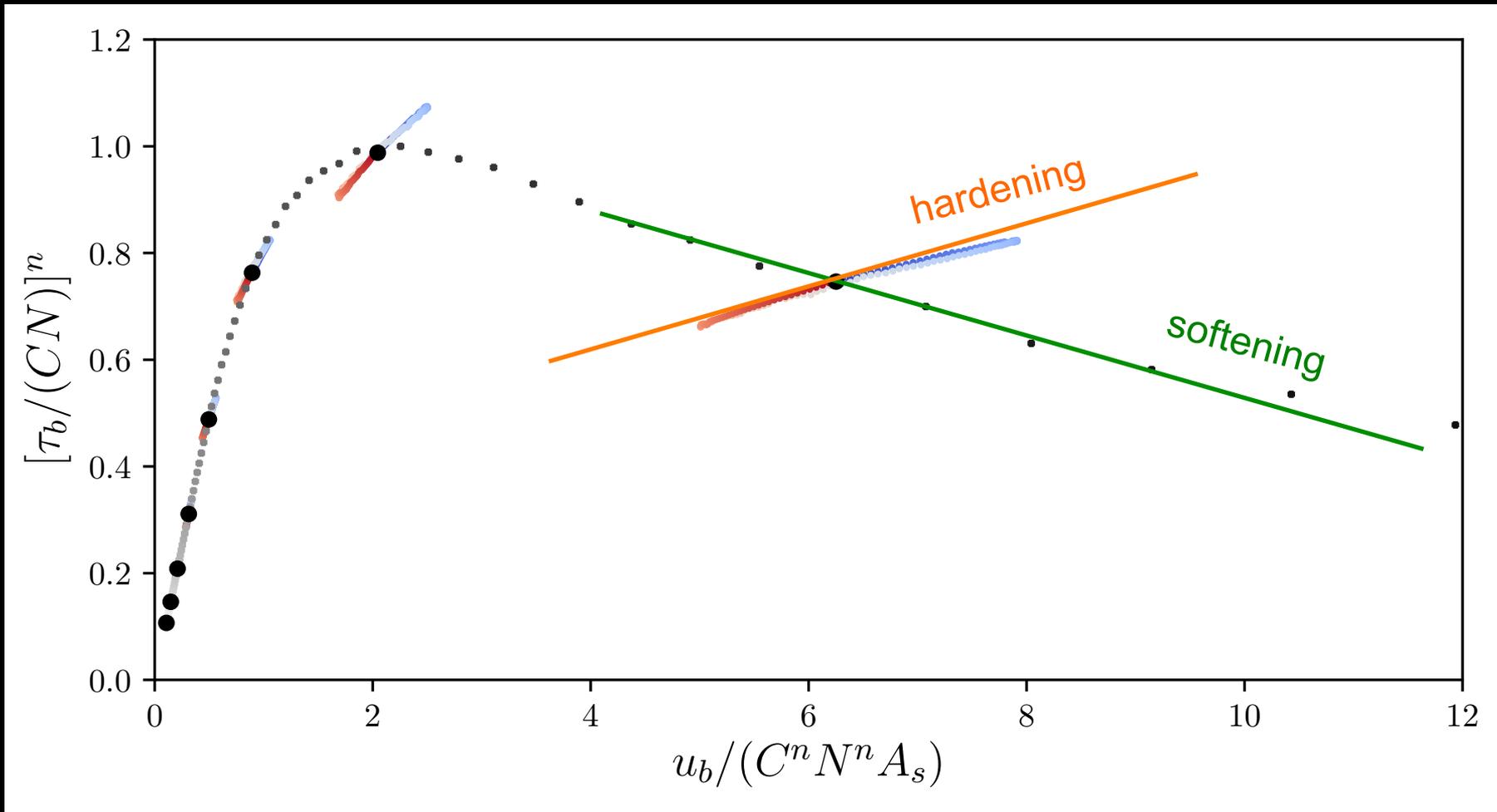
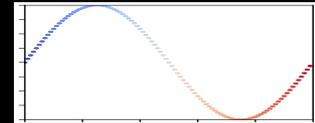
One year period

$$\Delta p_w / \bar{p}_i = 2\%$$



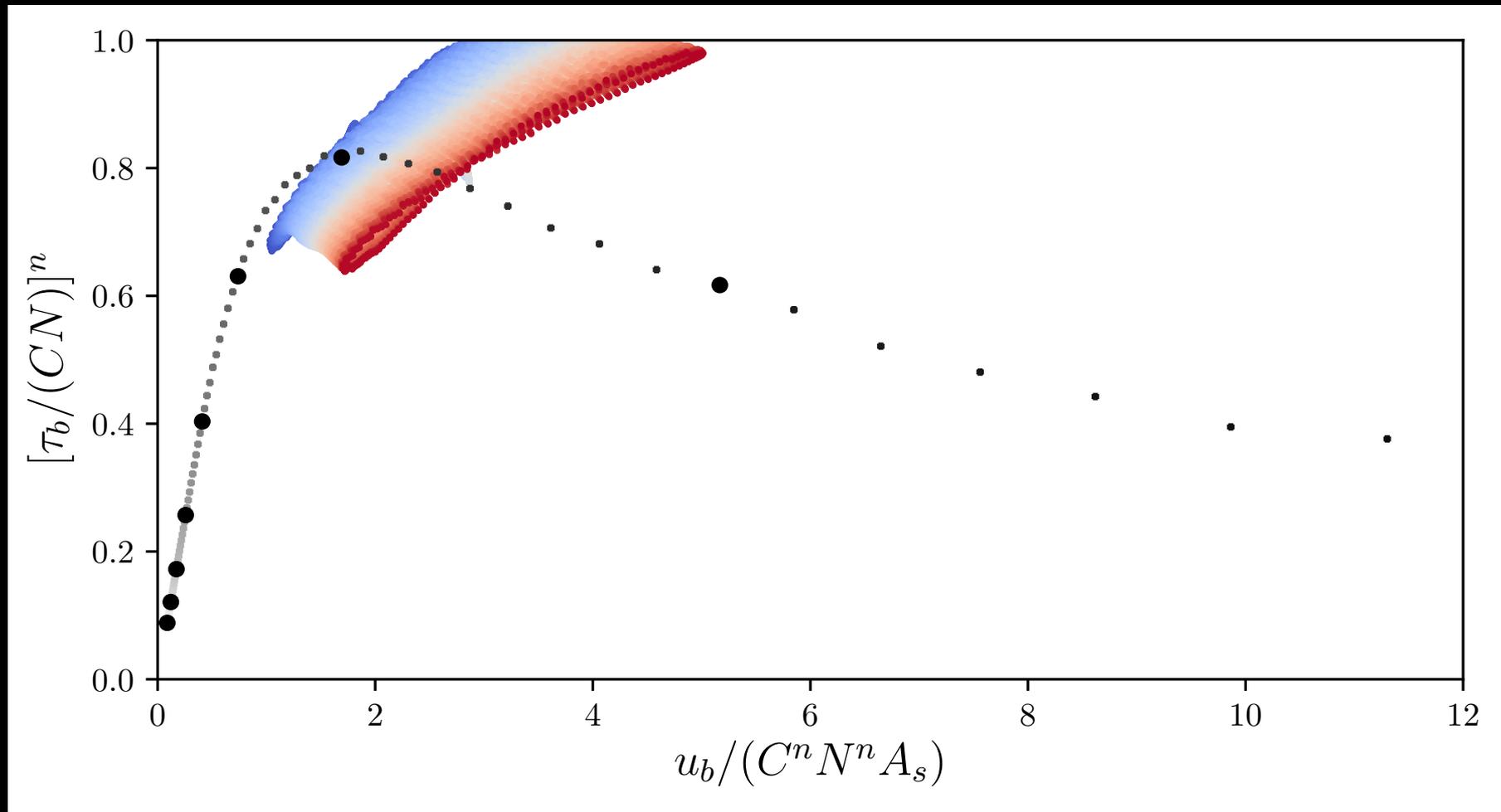
One day period

$$\Delta p_w / \bar{p}_i = 2\%$$

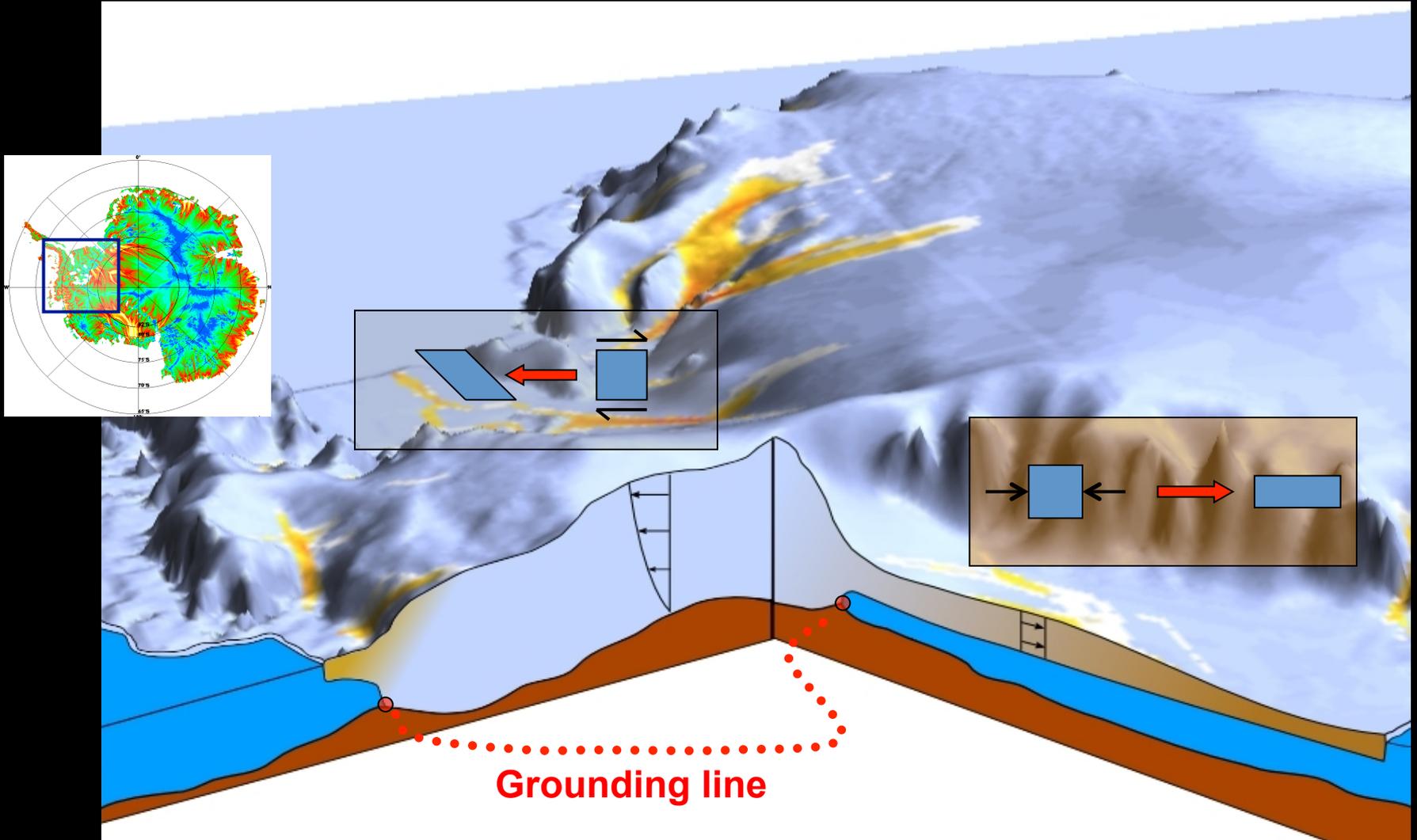


Year + day period

$$\Delta p_w / \bar{p}_i = 5\%$$



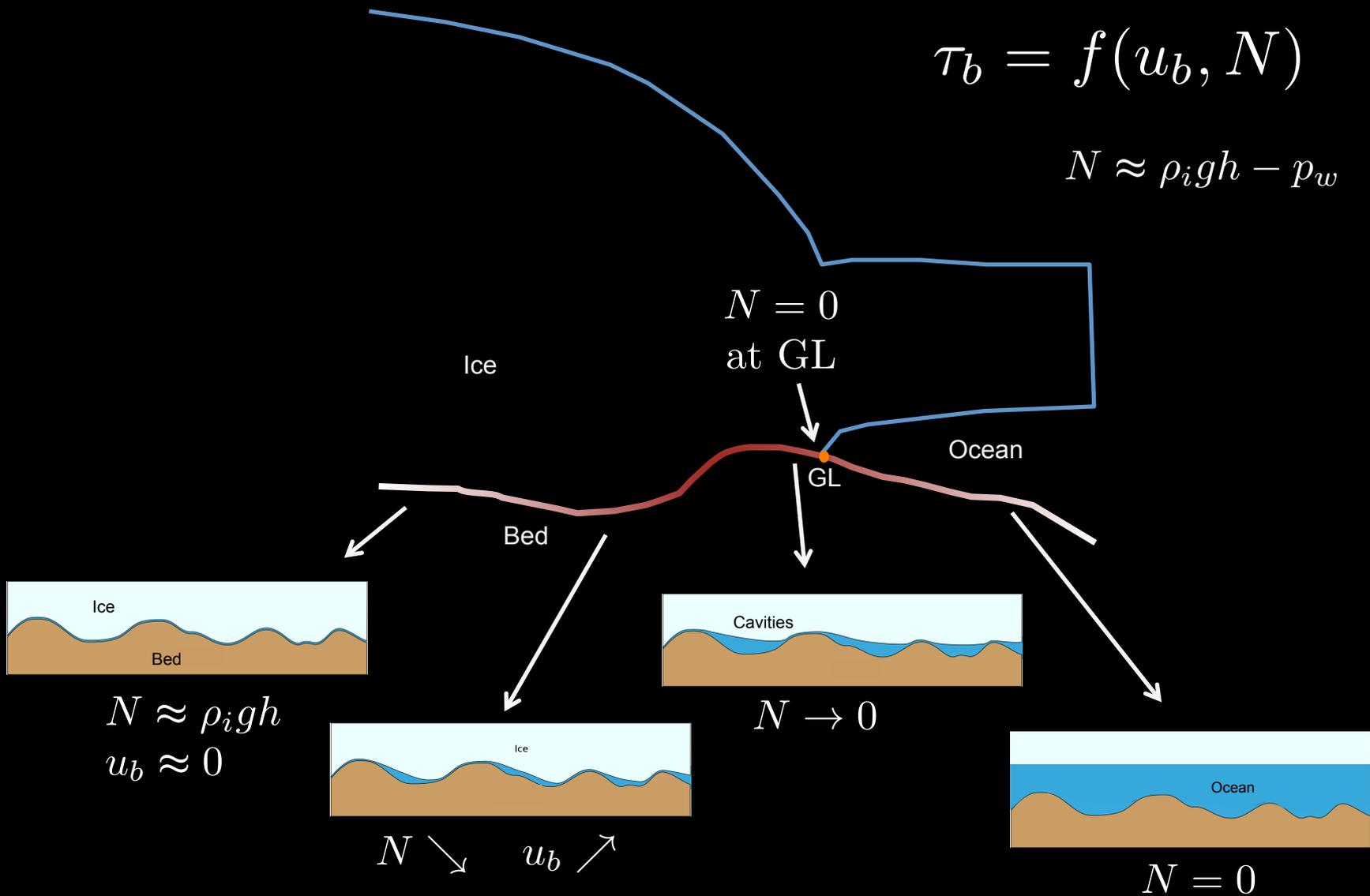
Grounding line



Types of basal conditions

$$\tau_b = f(u_b, N)$$

$$N \approx \rho_i g h - p_w$$



Which friction laws?

Isovalues of τ_b [MPa]

Weertman

$$\tau_b = C_W u_b^m$$

Coulomb

$$\tau_b = f_C N$$

Budd

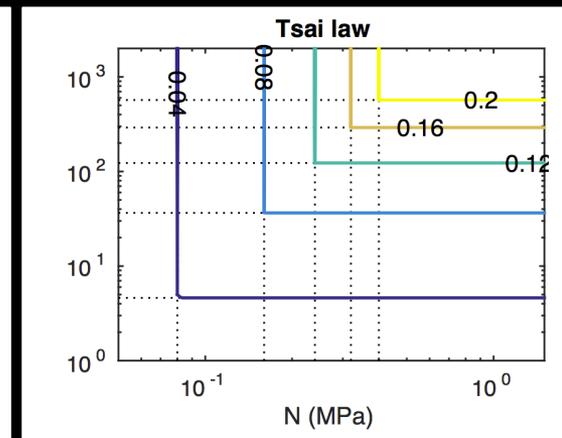
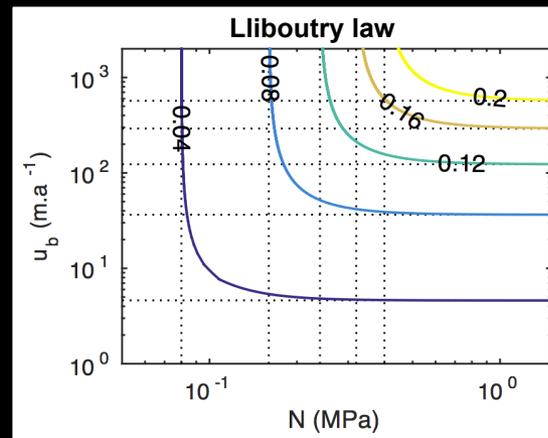
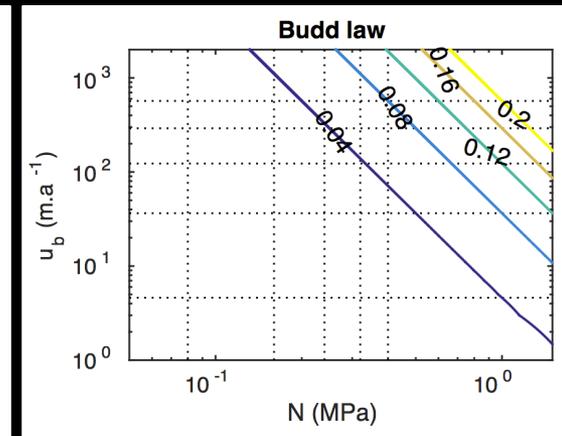
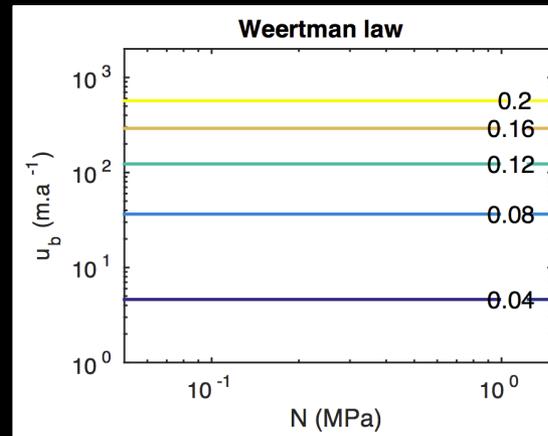
$$\tau_b = C_B u_b^m N$$

Liboutry

$$\tau_b = \frac{C_S u_b^m}{\left(1 + \left(\frac{C_S}{C_{\max} N}\right)^{1/m} u_b\right)^m}$$

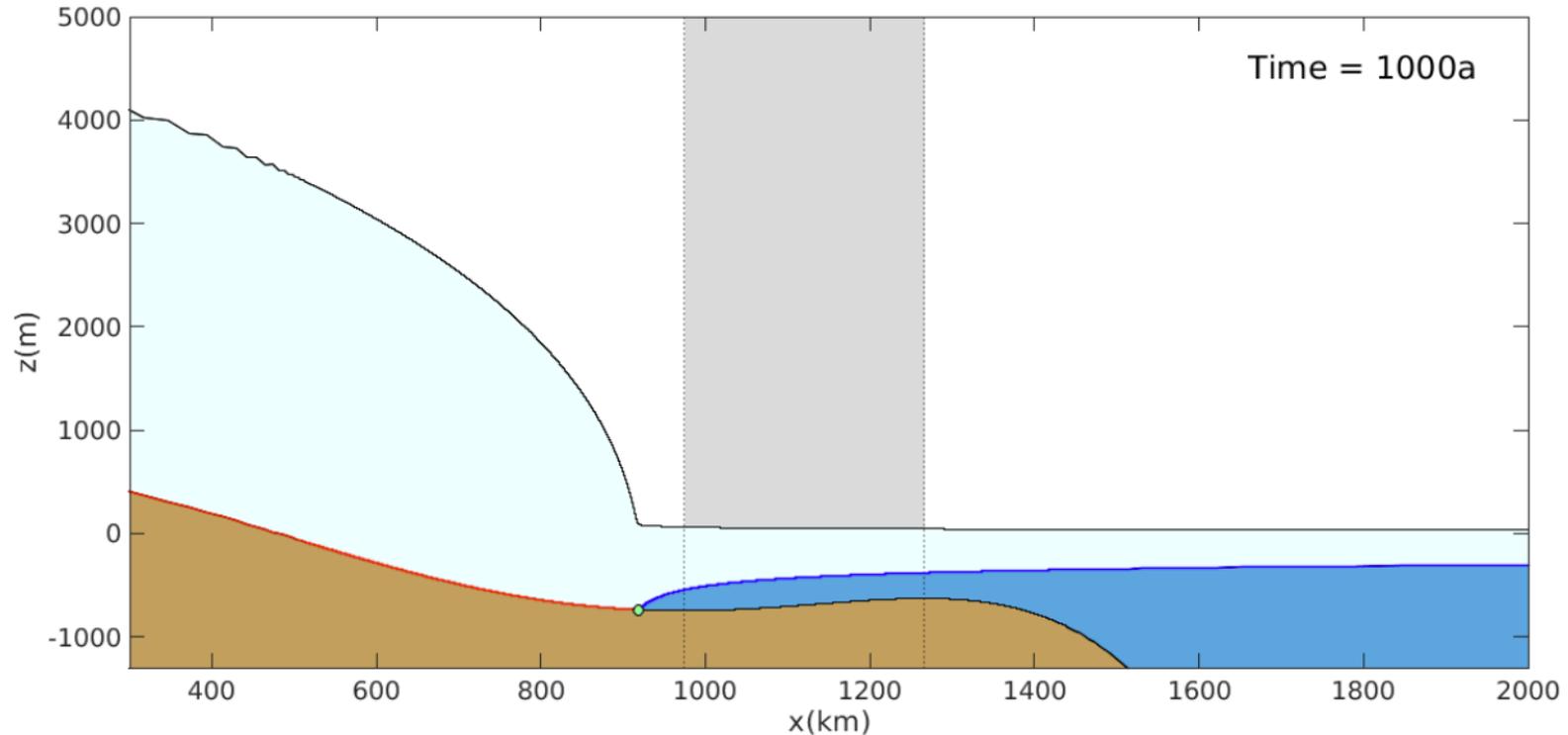
Tsai

$$\tau_b = \min [C_W u_b^m, f_C N]$$



$$m = 1/3, \quad C_W = C_B = C_S, \quad C_{\max} = f_C$$

2D exp - MISMIP setup



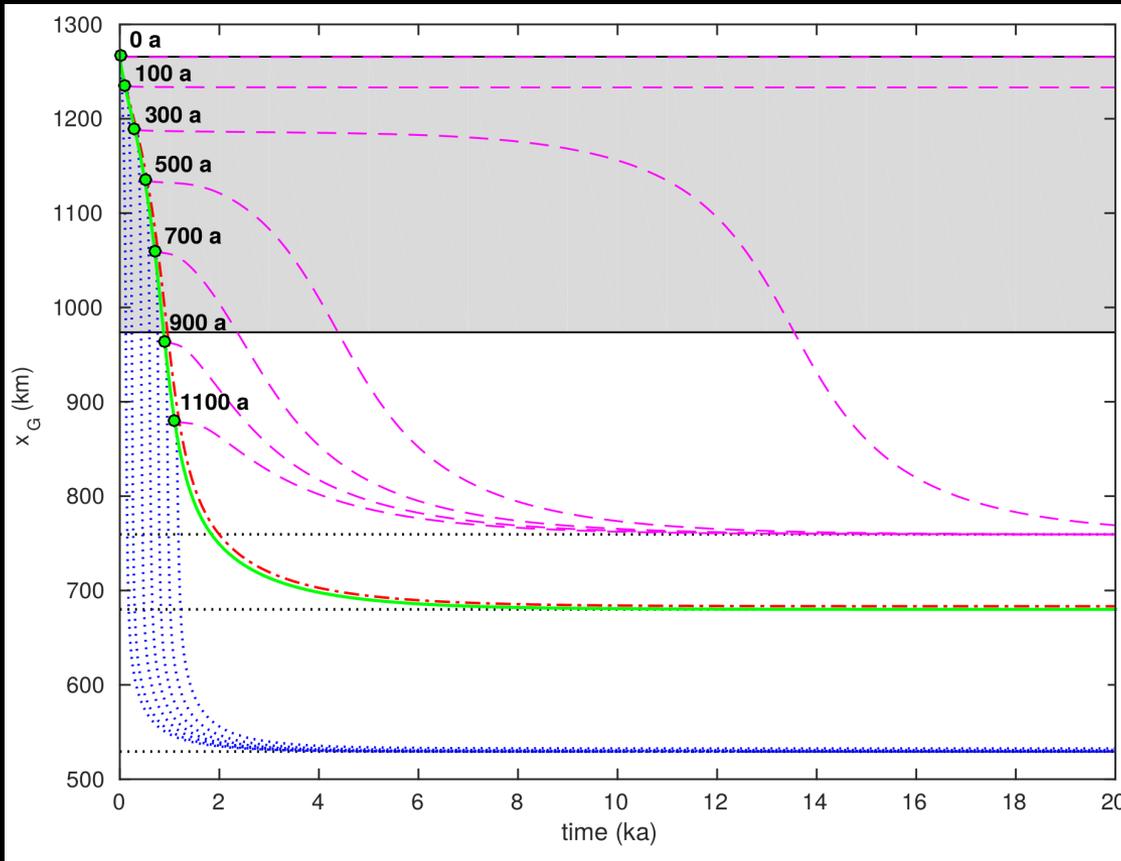
Assume $N = \rho_i g h - \rho_w g (Z_{sl} - Z_b)$

Use Liboutry solution as "observations"

Compare Weertman, Budd, Tsai to Liboutry

[Brondex et al., 2017]

2D exp - GL retreat speed



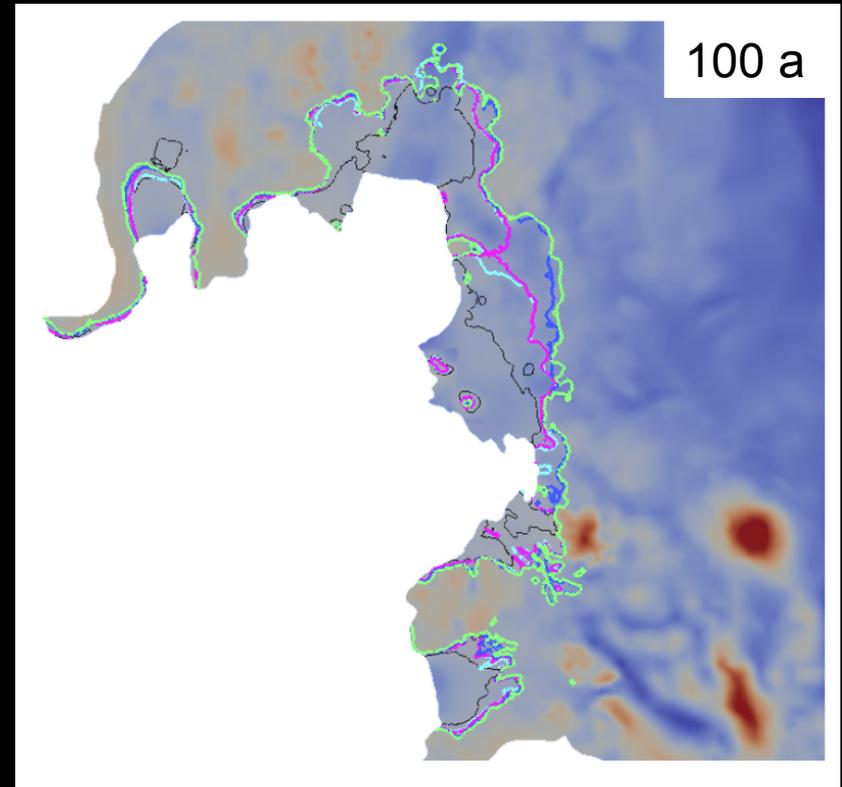
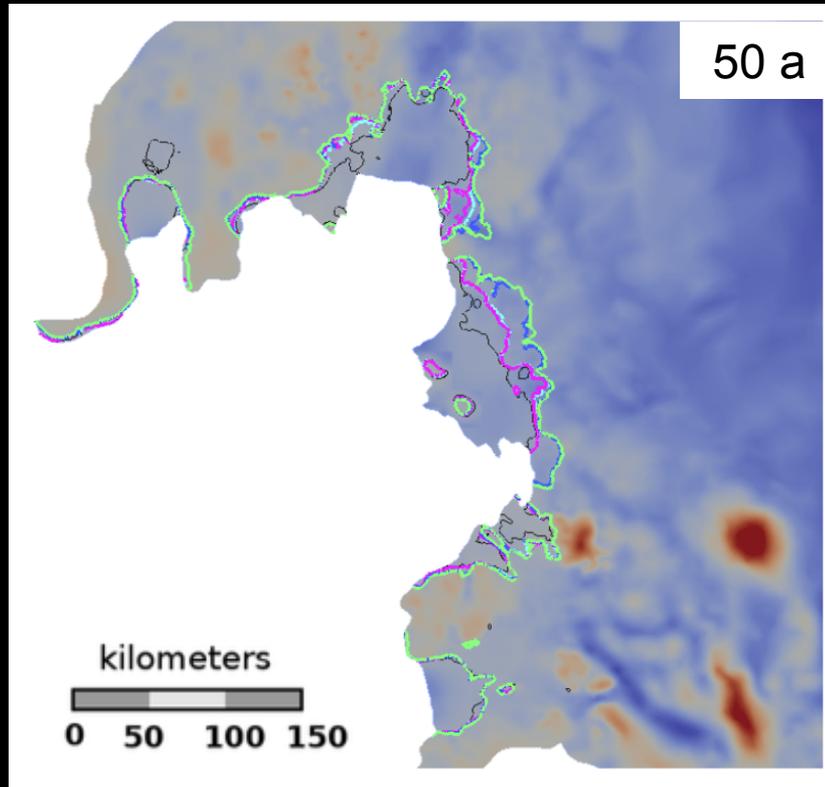
Weertman ~ 100 m/a

Liboutry / Tsai
 ~ 500 m/a

Budd ~ 9000 m/a

[Brondex et al., 2017]

Admundsen



Linear Weertman

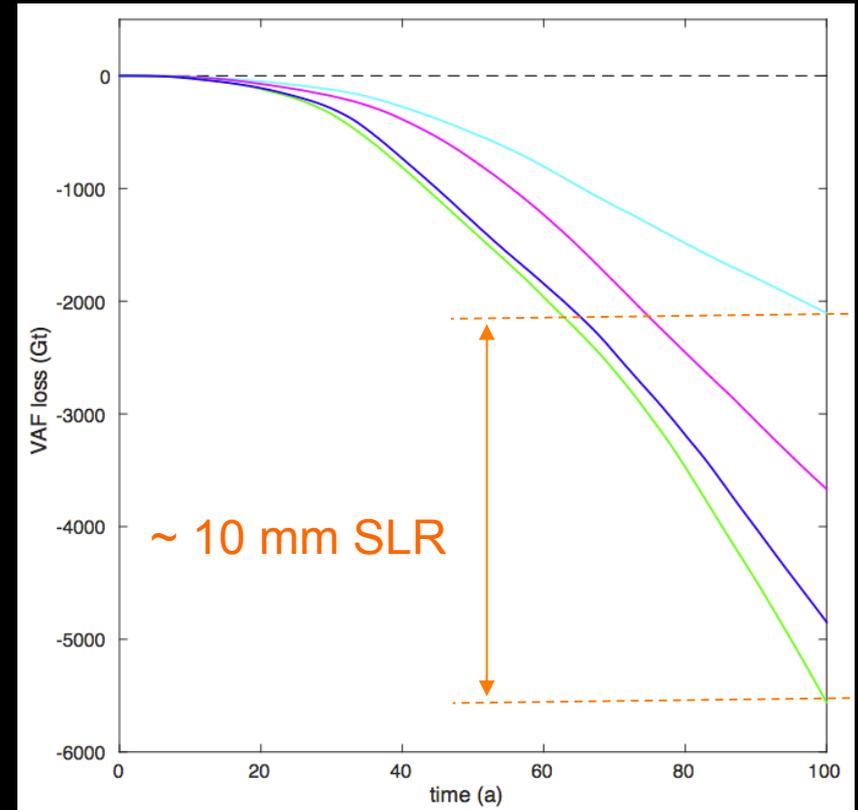
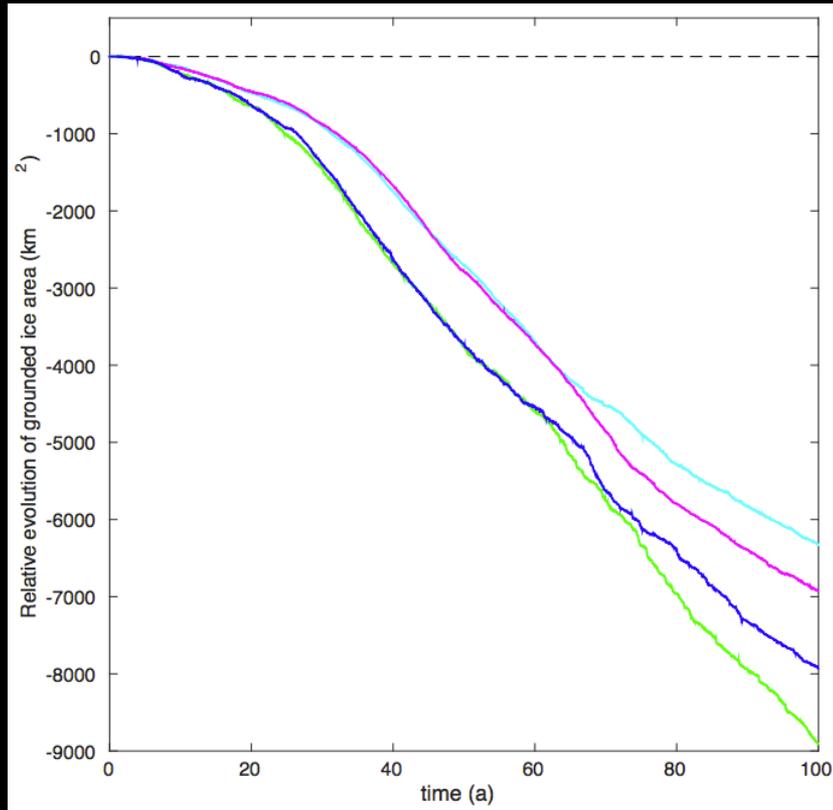
Non linear Weertman

Lliboutry $C_{max} = 0.4$

Lliboutry $C_{max} = 0.6$

[Brondex et al., 2019]

Admundsen - Results



Linear Weertman

Lliboutry C_{max} = 0.4

Non linear Weertman

Lliboutry C_{max} = 0.6

[Brondex et al., 2019]

Conclusions

- The ice dynamics strongly depend on the choice of the form of the friction law...
- and we are not yet sure what is the appropriate form for such friction law...
- more work to be done... on the path of Lliboutry and others

ANR SAUSSURE (2019-2023)

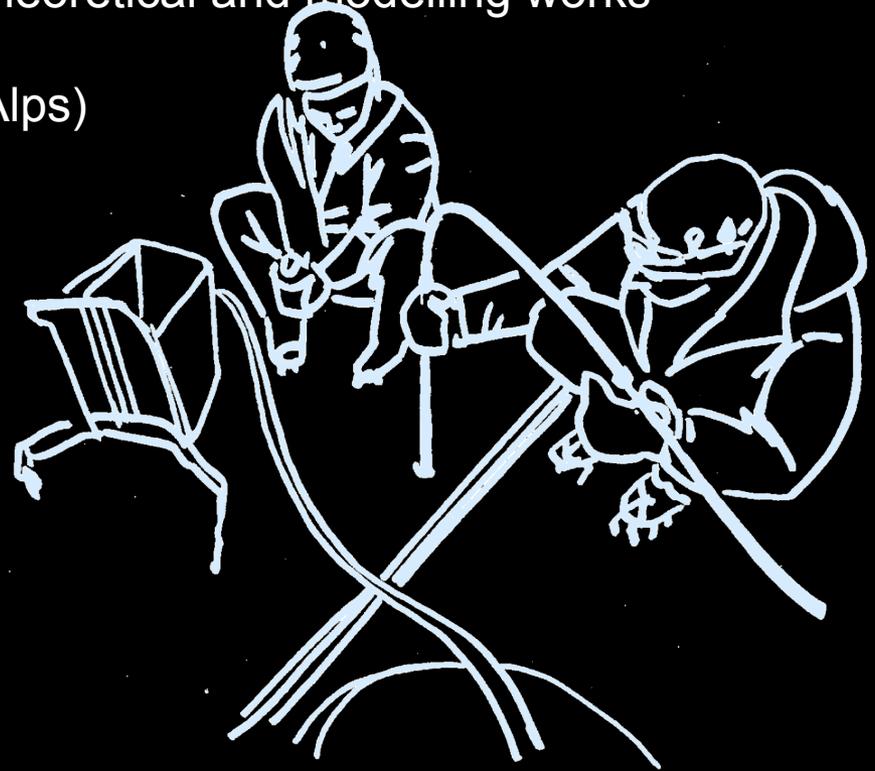
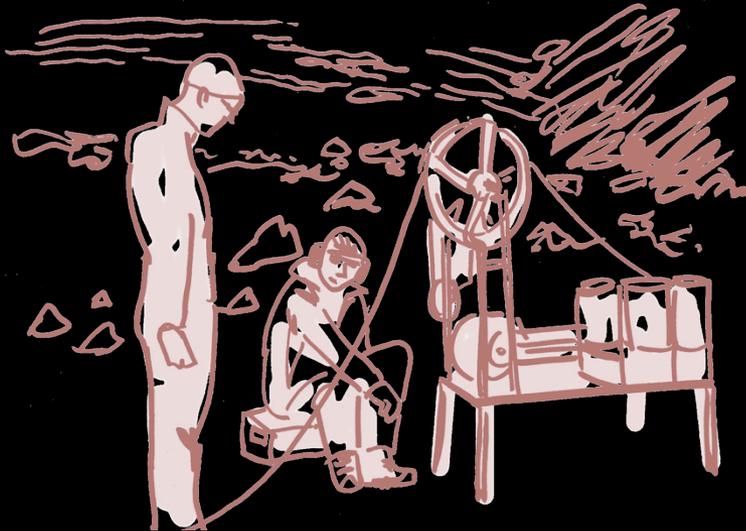


Objectives : evaluate, improve and validate various friction laws in a natural, geophysical scale configuration

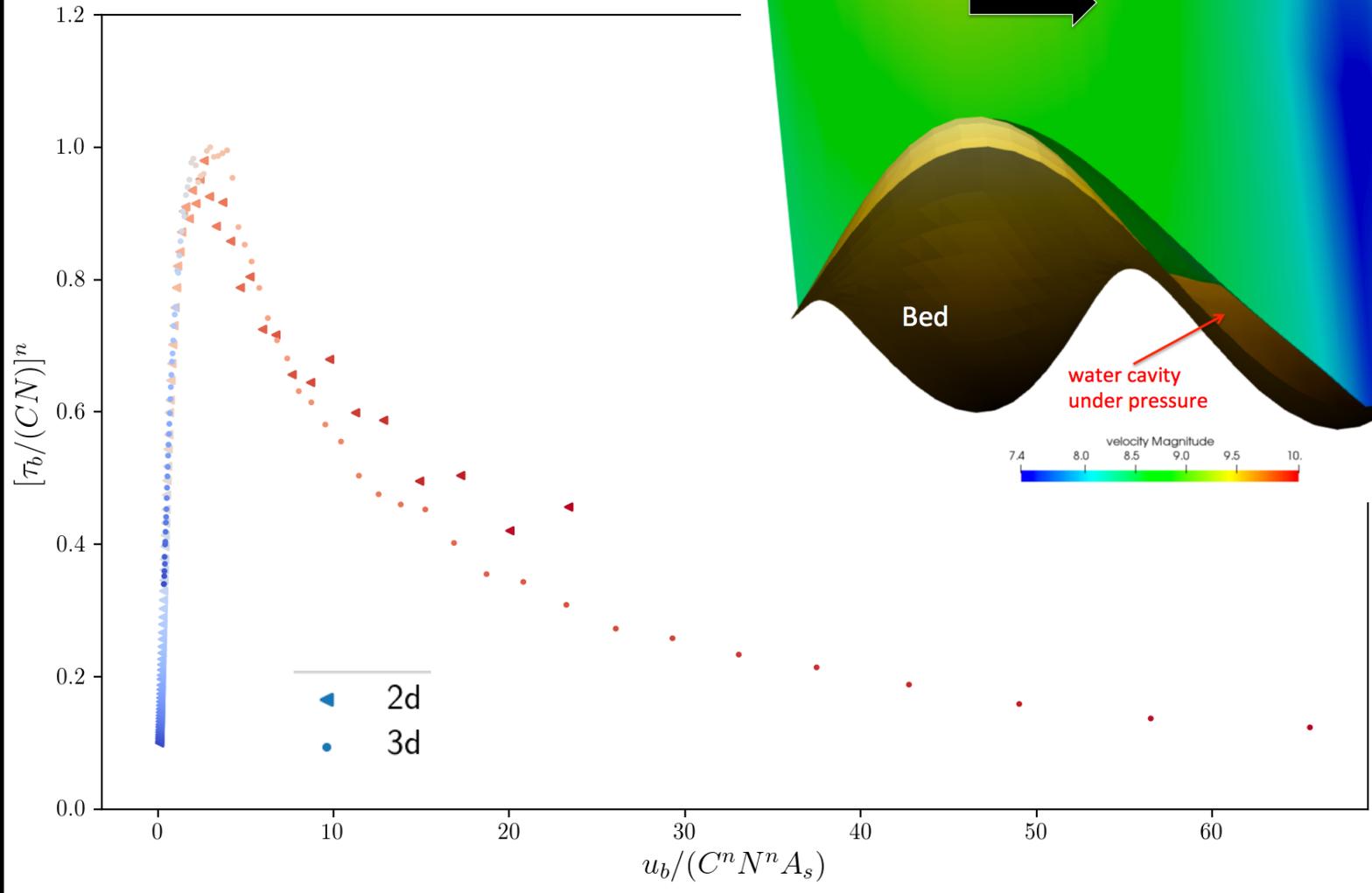
Methods : Observation combined with theoretical and modelling works

Site study : Argentière glacier (French Alps)

Involved lab : IGE, IRSTEA, IsTerre



3d effect (double sinus)



C value lower ; peak reached for lower water pressure

